

TECHNICAL REPORT

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Manipulating industrial robots — Informative guide on test equipment and metrology methods of operation for robot performance evaluation in accordance with ISO 9283

*Robots manipulateurs industriels — Guide informatif sur l'appareillage
d'essai et les méthodes métrologiques opératoires pour l'évaluation de la
performance d'un robot conformément à l'ISO 9283*

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Foreword

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The main task of ISO technical committees is to prepare International Standards. In exceptional circumstances a technical committee or sub-committee may propose the publication of Technical Report of one of following types:

- type 1, when the required support cannot be obtained for the publication of an International Standard, despite repeated efforts;
- type 2, when the subject is still under technical development or where for any other reason there is the future but not immediate possibility of an agreement on an International Standard;
- type 3, when a technical committee or sub-committee has collected data of a different kind from that which is normally published as an International Standard ("state-of-the-art", for example).

Technical Reports of types 1 and 2 are subject to review within three years of publication, to decide whether they can be transformed into International Standards. Technical Reports of type 3 do not necessarily have to be reviewed until the data they provide are considered to be no longer valid or useful.

ISO/TR 13309, which is a Technical Report of type 3, was prepared by Working Group 2 - Performance criteria and related testing methods - of ISO/TC 184/SC 2 - Robots for manufacturing environment.

This document is being published in the form of a Technical Report because it is intended to provide an overview on technically feasible metrology methods and the current state-of-the-art of test equipment when evaluating robot motion performances in accordance with ISO 9283:1990 - Manipulating industrial robots - Performance criteria and related test methods.

Introduction

The International Standards ISO 9283 and ISO 9946 were published in 1990 and 1991 in order to meet the needs of industries. For the purpose of supplementing these standards some amendments are being investigated for real applications.

It is important to clarify the kind and performance level of existing measurement systems applicable to robots in relation to ISO 9283 and establishing additional standards or reports.

This Technical Report contains an attempt to classify the measurement techniques and methods applicable to the robot characteristics testing, and describes the principles of operation and accuracies of the current state-of-the-art, and as much as possible, currently available measurement systems.

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Manipulating industrial robots — Informative guide on test equipment and metrology methods of operation for robot performance evaluation in accordance with ISO 9283

1. Scope

This report supplies information on the state-of-the-art of test equipment operating principles. Additional information is provided that describes the applications of current test equipment technology to ISO 9283.

2. Major categories of performance measuring methods

There are several methods which are used for characterizing robot performance in accordance with ISO 9283. These methods are classified as follows:

1. Positioning test probe methods
2. Path comparison methods
3. Trilateration methods
4. Polar coordinate measuring methods
5. Triangulation method
6. Inertial measuring method
7. Coordinate measuring methods
8. Path drawing method

Brief discussion of these methods is given in Section 4. Detailed description of these systems can be found in documents provided in Library list (Annex C).

3. Recommended robot performance measuring methods

Table 1 presents a list of the recommended methods for measuring the performance criteria in accordance with ISO 9283. The methods that are categorized into eight categories in Section 2 are itemized into a total of 16 individual methods. Each method's capabilities are also provided. Although some methods can be used to measure the characteristics of both the pose and the path, some of the methods have limitations. Some of the limitations are:

- (1) Only position (or orientation) can be measured in pose characteristics testing.
- (2) Path characteristics (linear or circular) can be measured only along restricted command paths.
- (3) Only robots with limited overshoot can be tested.
- (4) The performance of the test equipment may not provide sufficient accuracy or uncertainty of measurement for particular characteristics.

- (5) Measuring is limited to the number of freedom of the test equipment.
- (6) The test equipment may provide limited measurement volume compared to the test cube defined in ISO 9283.
- (7) The sampling frequency of the test equipment may not fit for the top frequency of the robot movement to be measured.

The tester should discuss the limitations with the test equipment manufacturer when planning performance measurement.

Table 2 is a summary of typical performance characteristics and capabilities of the recommended methods. It is advised that before testing a robot, the tester should understand the performance levels of the robot and select the appropriate testing methods.

4. Robot performance measuring methods

This section is a descriptive presentation and schematic configurations of the methods listed in Table 1.

4.1 Positioning test probe methods

The attained pose characteristics can be measured using a probe containing sufficient number of displacement or proximity sensors which are positioned by the robot to slowly touch a precision artifact located at a prescribed position or to stay in the air to measure possible overshoot. A typical set up is shown in Figure 1. Figure 2 shows some alternative applications of the method. Several types of test artifacts and probes can be combined, depending on the number of pose parameters required.

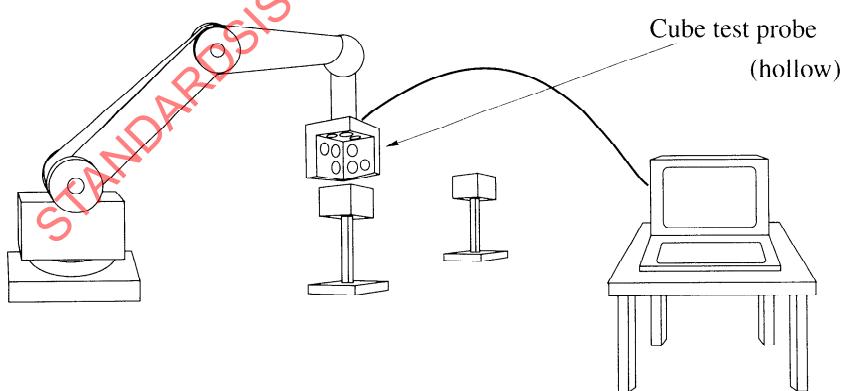


Figure 1 Positioning test probe method (cube artifact)

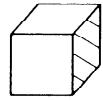
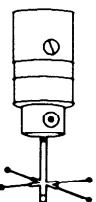
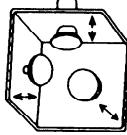
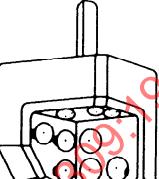
	Contact measurement (measuring x, y, z, coordinates)	Non-contact measurement (measuring x, y, z, a, b, c coordinates)	
Artifacts			
Examples of probe			
mounted on the robot			

Figure 2 Artifacts of positioning test probe method

4.2 Path comparison methods

4.2.1 Mechanical gage comparison

This method is based on comparing an attained path with a command path which could be composed of linear or circular path segments. The path is constructed using a precision mechanical gage or other position reference structure. Figure 3 shows a set up for the method where the proximity sensors are fitted on a cube probe and the artifact is a straight edge representing the command path. Deviations occurring during the execution of the path are sensed by appropriate number of sensors and used to determine characteristic parameters (accuracy and repeatability) of the attained path. Complete pose deviations (position and orientation) can also be determined when sufficient sensors are used.

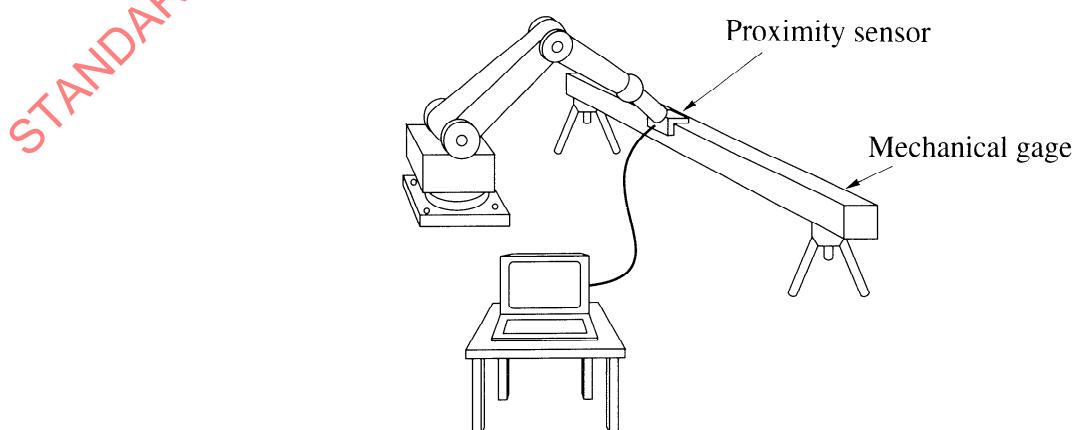


Figure 3 Mechanical gage comparison

4.2.2 Laser beam path comparison

Path accuracy/repeatability along a laser beam can be measured with a photosensitive transducer which has the capability of detecting the position error of incident beam from the centre of the transducer. System set up is shown in Figure 4.

The robot's pose along the beam can be calculated as a function of time if the laser source is replaced by a laser interferometer and the photosensitive transducer has light reflecting capability.

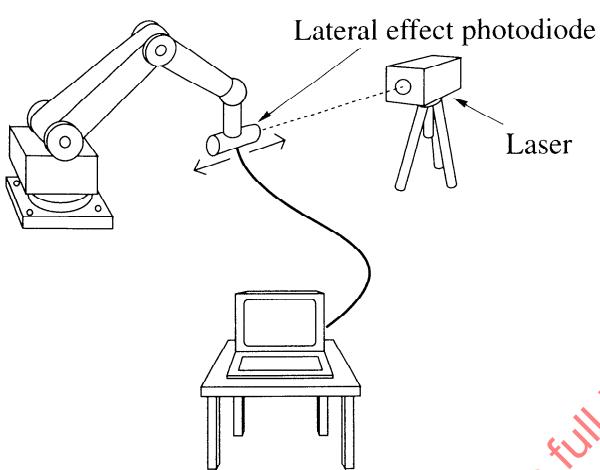


Figure 4 Laser beam path comparison

4.3 Trilateration Methods

Trilateration (meaning "using three sides") is a method of determining the Cartesian coordinate (x , y , z) of a point P in three-dimensional space with three distance values between the point P and the three observation stations, and the base lengths between three fixed stations. Figure 5 explains the principle of trilateration in two-dimensional representation.

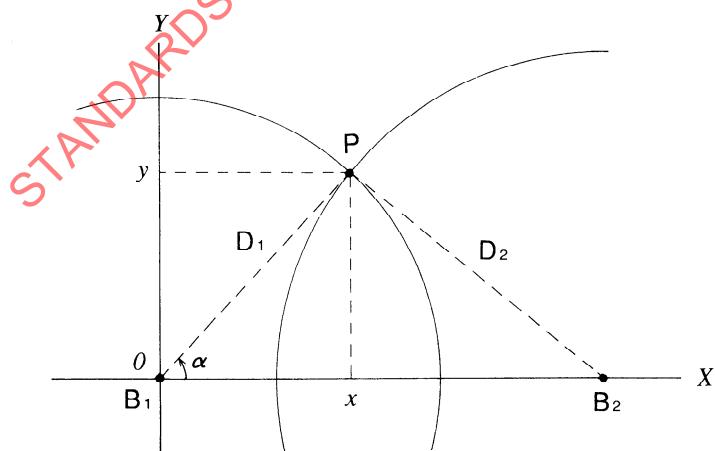


Figure 5 Measuring principle of trilateration
(two-dimensional representation)

4.3.1 Multi-laser tracking interferometry

This method is based on using three laser beams produced from three laser interferometers with two-axis servo controlled tracking aimed at a common target located on the robot's wrist. System set up is shown in Figure 6. The Robot pose characteristic in three-dimensional space can be determined based on distance data obtained from the three interferometers. The orientation can be measured if six interferometers are used in a set up in which the six beams are aimed at three independent targets on the robot.

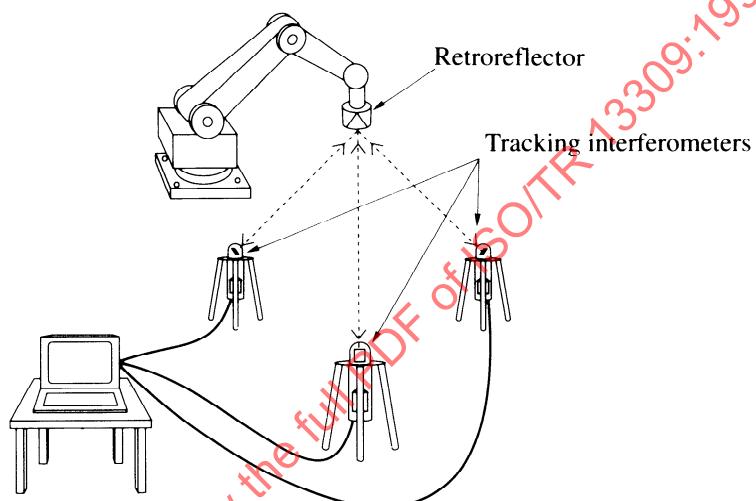


Figure 6 Multi-laser tracking interferometry

4.3.2 Ultrasonic trilateration

The robot's position in three-dimensional space can be calculated with distance data from three stationary ultrasonic microphones which receive ultrasonic pulse trains from a sound source mounted on the robot. System set up is shown in Figure 7.

The robot's orientation can be measured if the robot has three independent sound sources and each stationary microphone can detect pulse trains from all three sound sources.

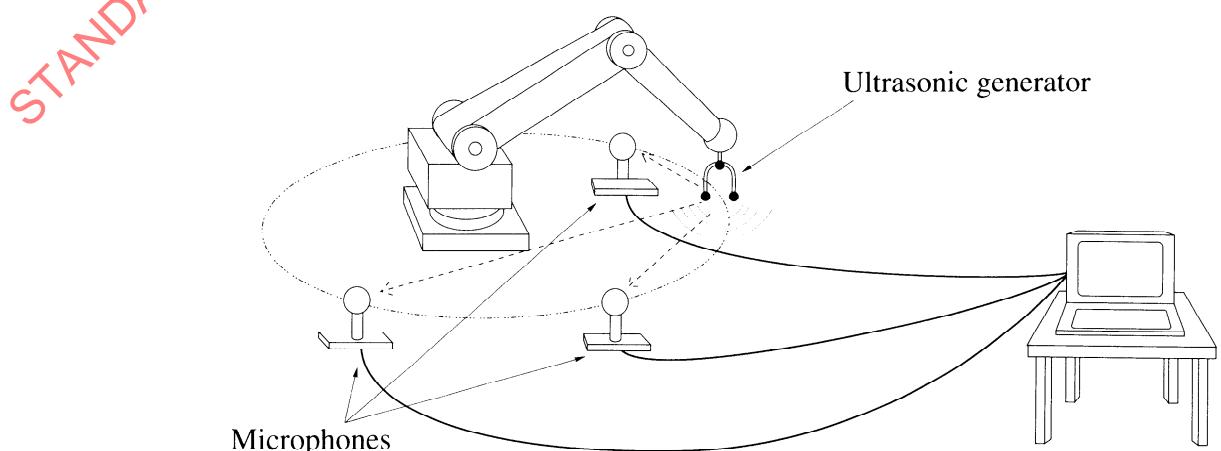


Figure 7 Ultrasonic trilateration

4.3.3 Mechanical cable trilateration

This method is based on connecting three cables originated from three fixed cable-feeding devices to the robot's end point as shown in Figure 8. By evaluating the length of each cable, such as using potentiometers or encoders on the cable feeding devices which maintain the cables under tension, the position of the robot's end point can be determined.

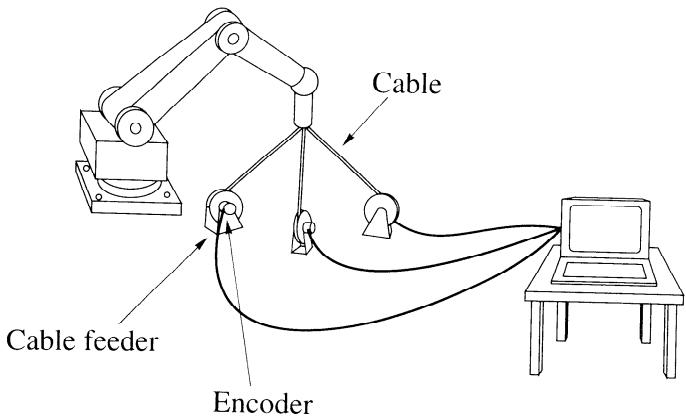


Figure 8 Mechanical cable trilateration

4.4 Polar coordinate measuring methods

Polar coordinate measuring methods can be used to determine the Cartesian coordinate (x, y, z) of a point in space by measuring a distance D , azimuth (α) and elevation (β) values as shown in Figure 9.

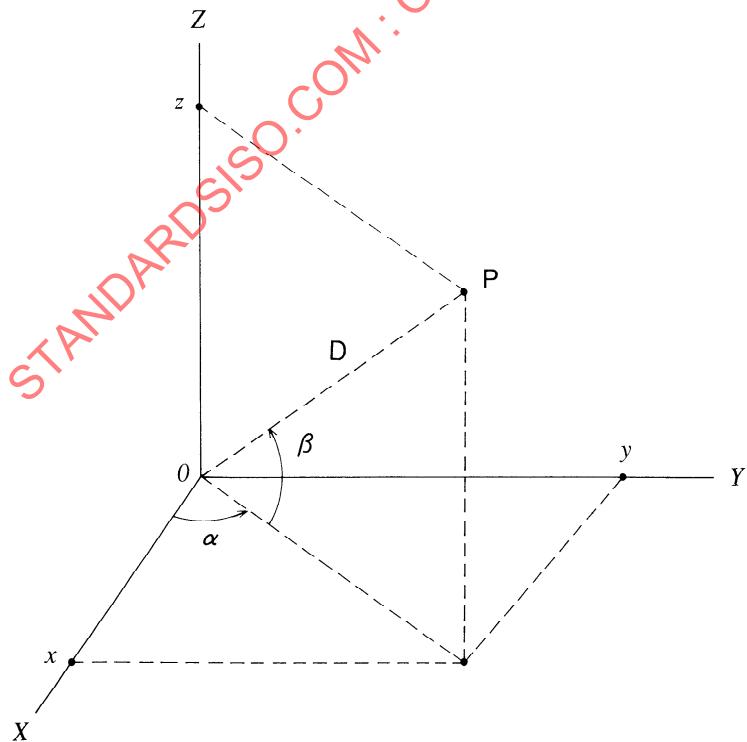


Figure 9 Principle of three-dimensional polar coordinate measuring

4.4.1 Single laser tracking interferometry

Laser tracking interferometry method can be used to measure robot's position or orientation. Figure 10 shows a typical setup of a single laser interferometer for position measurement. The robot's position can be calculated with distance data from the laser interferometer and azimuth/elevation data which is obtained from a stationary tracking system aimed at a retroreflector mirror mounted on the robot's end point.

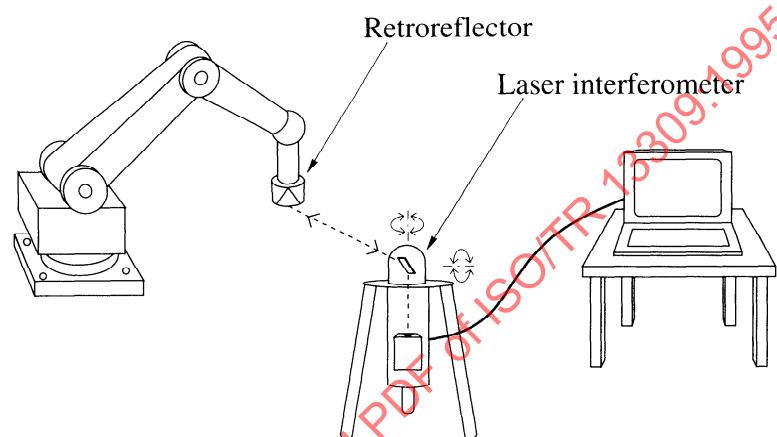


Figure 10 Single laser tracking interferometry for position measurement

The robot's orientation (pitch and yaw) can also be measured using the same system (Figure 11), if the retroreflector mirror system has the capability of keeping its optical axis pointed to the stationary tracking system, or if the stationary tracking system can analyze the diffracted image reflected by the retroreflector. This method can test 6 DOF (degree of freedom) robots.

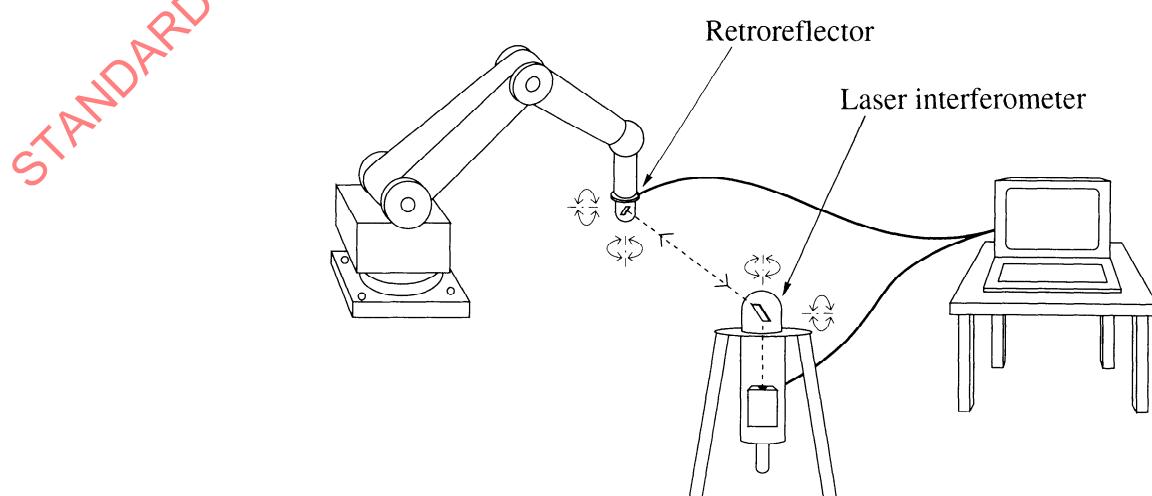


Figure 11 Single laser tracking interferometry for pose measurement

4.4.2 Single total station method (static/tracking)

The robot's attained position can be measured by a static total station (capable of measuring distance, azimuth and elevation) point by point.

The robot's attained pose (positioning factor) or attained path (positioning factor) can also be measured by a tracking total station which keeps track of a moving retroreflector mounted on the robot. Figure 12 shows a typical set up for the system.

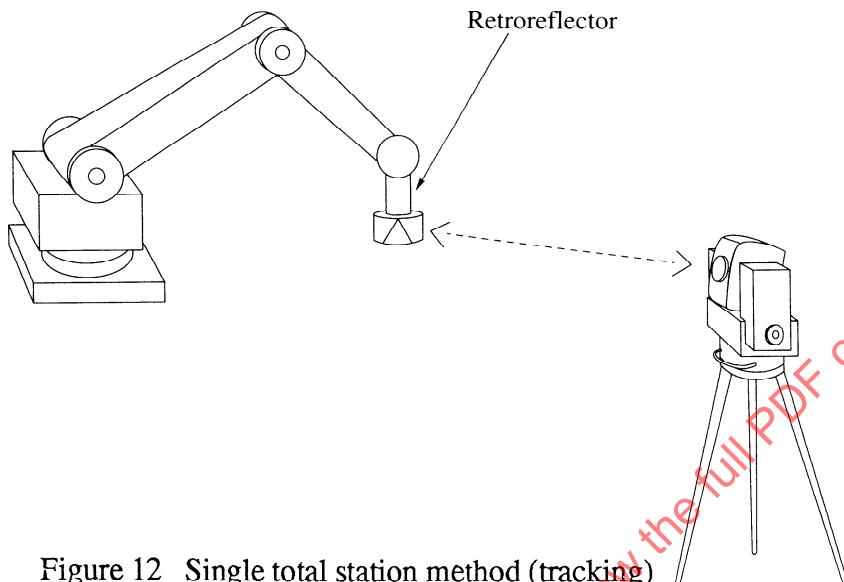


Figure 12 Single total station method (tracking)

4.4.3 Linear scale method

The robot's position can be measured as a function of time with distance data and azimuth/elevation data from a linear scale.

In the linear scale method, shown in Figure 13, the upper end of the linear scale is joined to the robot, and the distance between the upper end and the point connected at the encoders is measured.

Azimuth/elevation data pointing the upper end of the linear scale are obtained with one encoder moving horizontally and the second encoder moving vertically.

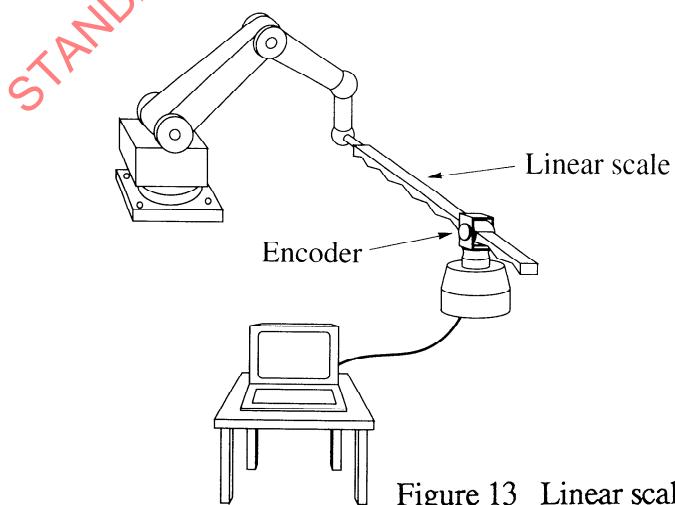


Figure 13 Linear scale method

4.5 Triangulation methods

Triangulation is a method which can be used for determining the position of a point in space. In two-dimensional triangulation, the Cartesian coordinates (x , y) of point P (See Figure 14) can be determined with the base line length B_1B_2 , two azimuths α_1 and α_2 .

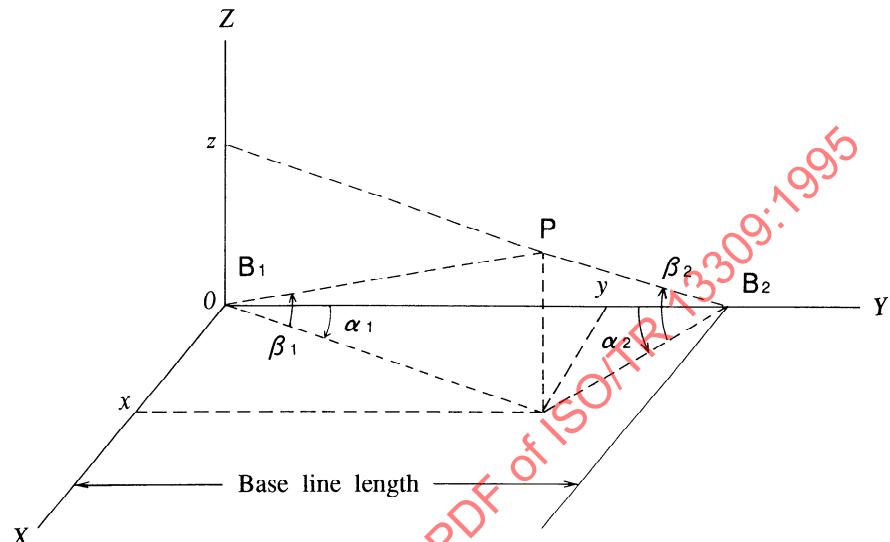


Figure 14 Measuring principle of triangulation

4.5.1 Optical tracking triangulation methods

In these methods, the robot position can be determined as a function of time with two sets of azimuth/elevation data from two two-axis optical tracking systems. Thus, these methods can be used for both static and dynamic measurements. Figures 15, 16 and 17 show typical configurations of three common optical tracking triangulation systems.

In the laser tracking system, shown in Figure 15, two laser beams from two tracking systems are continuously aimed at a reflector mounted on the robot end point. The laser scanning method, shown in Figure 16, is another method of determining the robot's position. The method is based on detecting the incident light on a robot mounted target from three laser scanners which emit line-projected light. Two scanners project the vertical lines and the third scanner emits the horizontal line.

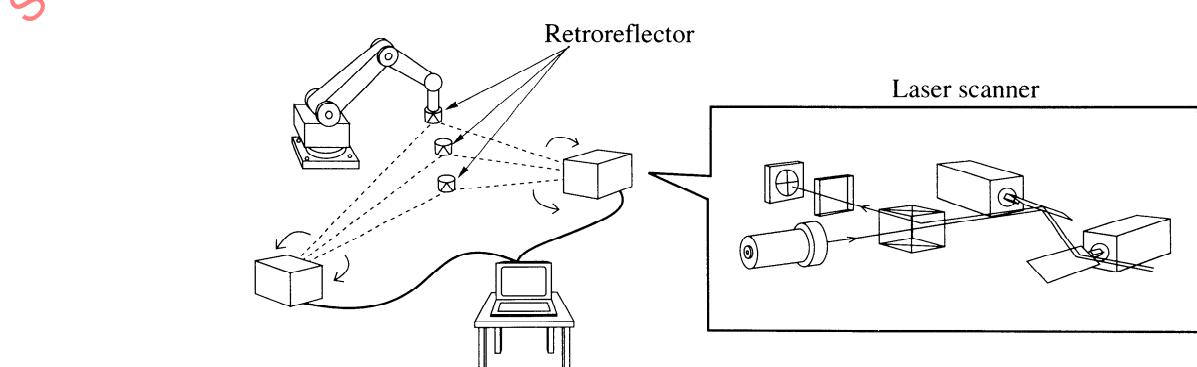


Figure 15 Laser tracking triangulation system

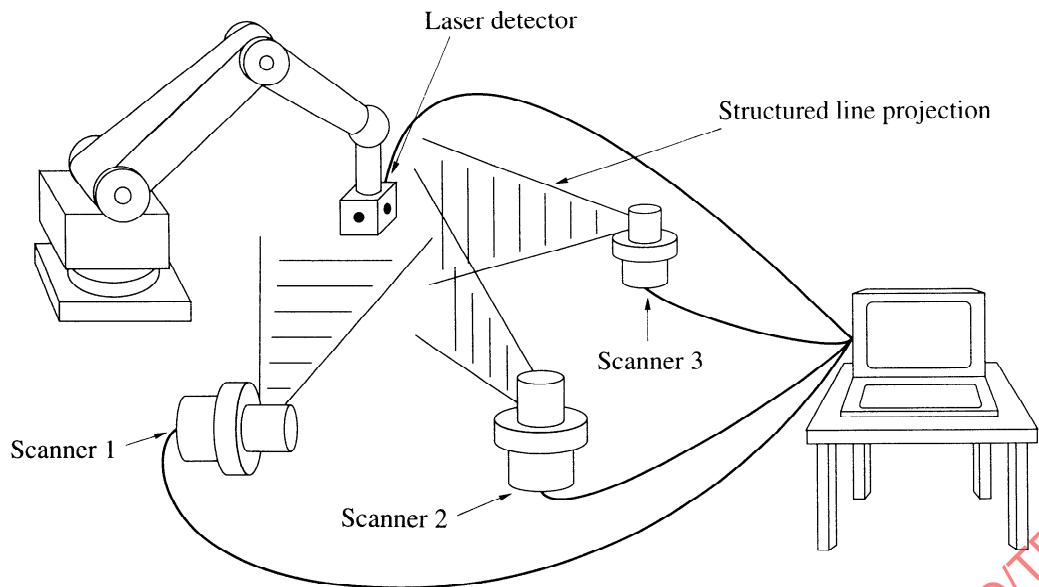


Figure 16 Laser scanning triangulation system

The robot's orientation can be calculated if two structured laser beams (cross shape) track a cubic probe equipped with two CCD ring sensors on the adjacent surfaces of the probe (Figure 17).

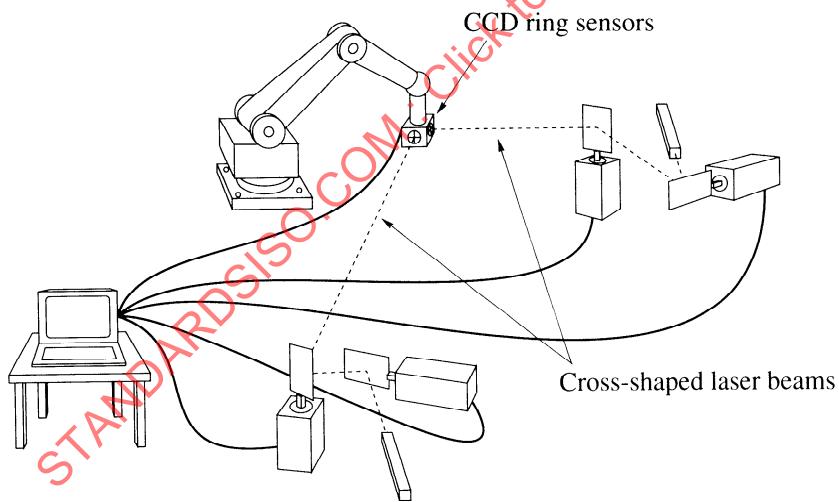


Figure 17 CCD ring and laser tracking triangulation system

4.5.2 Theodolite method

The robot attained position can be determined with two sets of azimuth/elevation data by using two (or more) stationary theodolites with their beams aimed at a target mounted on the robot end point. Typical set up is shown in Figure 18. The orientation can be calculated if the robot has multiple target points. Manual theodolites are useful only for static measurements since they are manually operated.

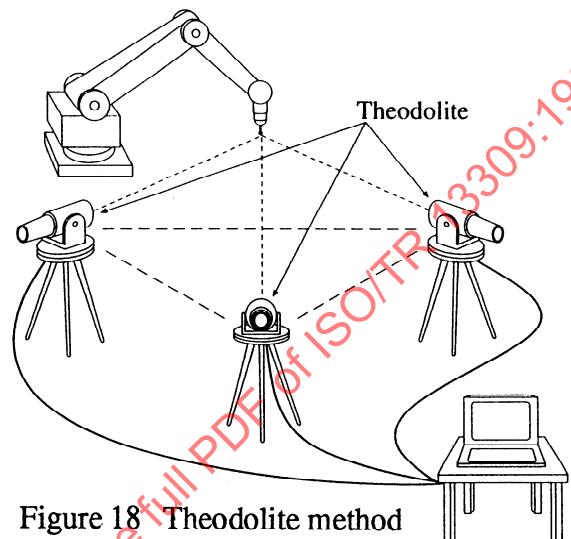


Figure 18 Theodolite method

4.5.3 Optical camera method

The robot's position can be measured as a function of time with image captured by two imaging devices (one-dimensional or two-dimensional).

The robot's orientation can be determined as a function of time if multiple light sources or multiple targets are mounted on the robot to be monitored by the imaging devices.

During measurement light sources on the robot are sequentially turned on to know from which light source the image comes.

This method uses two imaging devices (cameras) located at a fixed known distance. Figure 19 is a typical set up for the system. The cameras monitor an illuminating target fixed to the robot end point. Position sensing devices (or CCDs) are used to determine the positions of target in the camera coordinate system. This information, together with knowledge of distance between cameras, allows the determination of the target position.

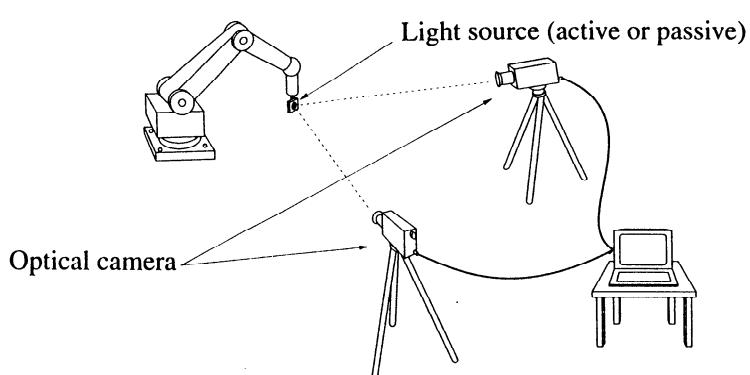


Figure 19 Optical camera method

4.6 Inertial measuring method

The robot's pose characteristics and path characteristics can be measured in all of three directions in space by three servo acceleration sensors and three gyroscopes mounted on the robot without any external observation installations when the robot's initial state is known. Figure 20 is a typical set up for the system.

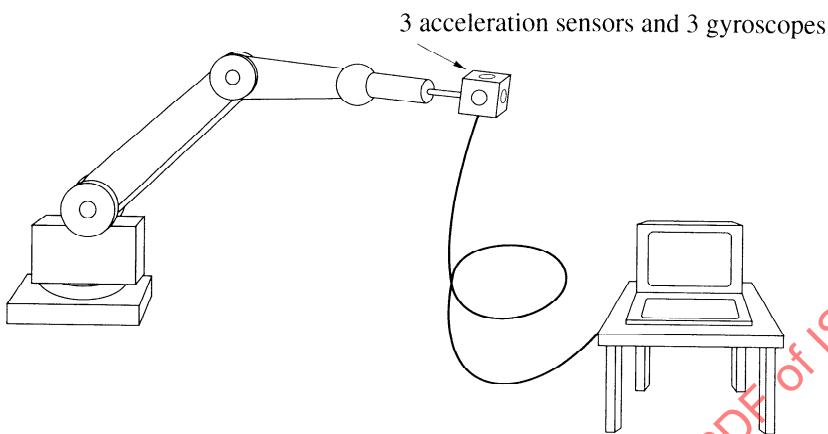


Figure 20 Inertial measuring method

4.7 Coordinate Measuring Methods (Cartesian)

4.7.1 Two-dimensional digitizing method

The robot's planar position can be measured as X-Y, Y-Z or Z-X coordinate values with a high resolution camera mounted on the robot. Typical system set up is shown in Figure 21. The camera counts high precision scale lines on the plate which constitutes the lines of the test plane.

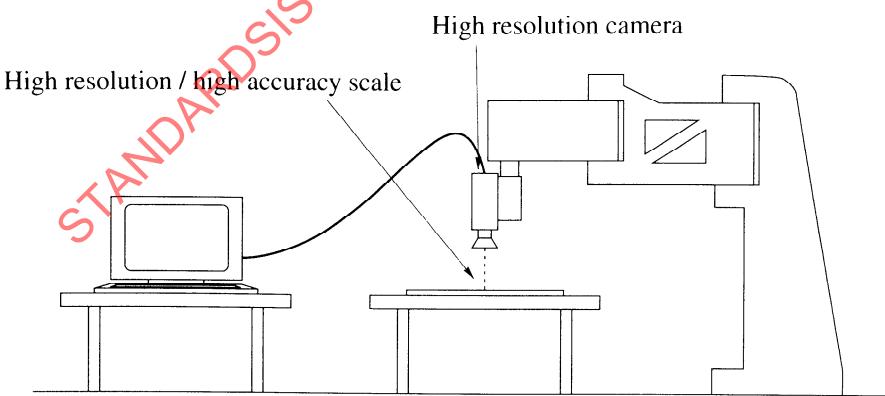


Figure 21 Two-dimensional digitizing method 1

The robot's planar position in limited area can be measured with the interferential measuring principle with sub-micrometer resolution. Moiré patterns generated on the cross grid plate are captured by the scanning head and are analysed to give 2-dimensional incremental values (Figure 22).

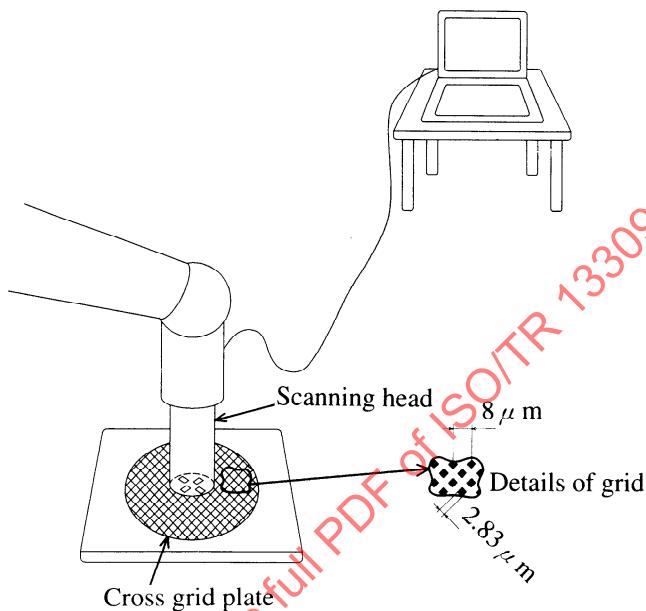


Figure 22 Two-dimensional digitizing method 2

The robot's position can be measured as X-Y, Y-Z or Z-X coordinate values with a digitizing pen mounted on the robot and a tablet set as the test plane (Figure 23). This method can be used for point to point calibration or continuous path motions. Thus, it is used for both static and dynamic measurements.

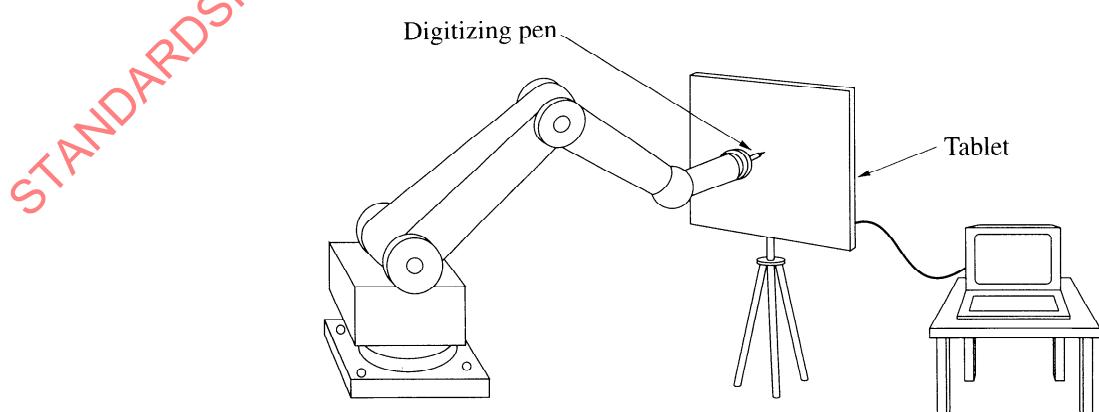


Figure 23 Two-dimensional digitizing method 3

4.7.2 Coordinate measuring machine method

The robot's attained position can be measured by getting coordinate values of the robot target point with a coordinate measuring machine (Figure 24). The robot's attained orientation can be measured by obtaining coordinate values of three or more points by touching a cubic target.

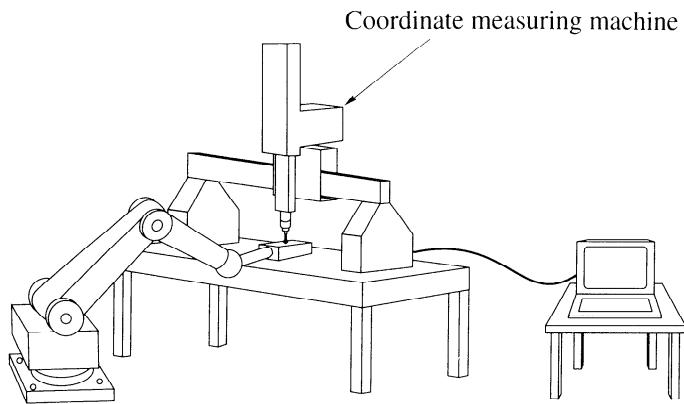


Figure 24 Coordinate measuring machine method

4.8 Path drawing method

The two-dimensional path of the robot can be recorded on paper with mechanical, electric or ink jet pens. Figure 25 represents an example which uses electric discharge paper typical in facsimile recording. The robot velocity characteristics can be measured if timing pulses are generated.

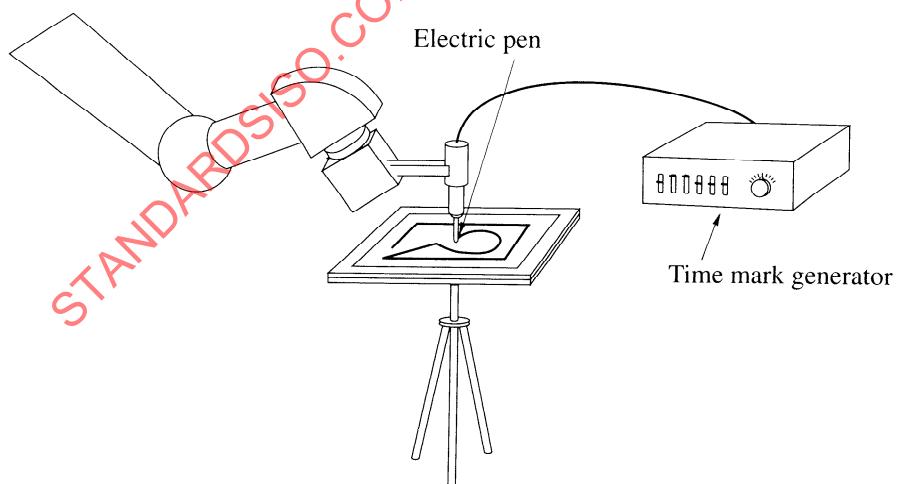


Figure 25 Path drawing method

Table 1. Measuring methods of robot performance characteristics

Performance characteristics		Measuring methods														
◎	These systems have the capability of calibrating both the measuring system itself and the robot base coordinate system. This also means that these systems can measure both absolute accuracy (pose, path) and relative accuracy (pose, path).	4.1	Positioning test probe methods	4.1.1	Cube artifact	□	○	○	○	○	○	○	○	○	○	
□	These systems can measure only relative accuracy (pose, path).	4.1.2	Ball artifact	□	△	△	△	△	△	△	○	○	○	○	○	
○	Robots with average performances can be tested with this method.	4.2	Path comparison methods	4.2.1	Mechanical gage comparison method	△	△	△	—	—	—	—	—	—	—	
△	Performances can be measured with some limitations. See Clause 3.	4.2.2	Laser beam path comparison method	△	△	○	○	○	○	—	—	—	—	—	—	—
—	This method is not suitable for testing the criteria.	4.3	Trilateration methods (distance – distance)	4.3.1	Multi-laser tracking interferometry	○	○	○	○	○	○	○	○	○	○	○
		4.3.2	Ultrasonic trilateration	△	△	△	△	△	△	△	○	○	○	○	○	○
		4.3.3	Mechanical cable trilateration	△	△	△	○	○	○	○	○	○	○	○	○	○
		4.4	Polar coordinate measuring methods (distance – azimuth)	4.4.1	Single laser tracking interferometry	○	○	○	○	○	○	○	○	○	○	○
		4.4.2	Single total station method – tracking	○	○	○	○	—	—	○	○	—	—	—	—	—
		4.4.3	Linear scale method	△	△	△	△	△	△	△	○	○	○	○	○	○
		4.5	Triangulation methods (azimuth – azimuth)	4.5.1	Optical tracking triangulation methods	○	○	○	○	○	○	○	○	○	○	○
		4.5.2	Theodolite method	○	○	○	○	—	—	○	—	—	—	—	—	—
		4.5.3	Optical camera method	○	○	○	○	○	○	○	○	○	○	○	○	○
		4.6	Inertial measuring method	□	○	○	○	○	○	○	○	○	○	○	○	○
		4.7	Coordinate measuring methods (Cartesian)	4.7.1	Two-dimensional digitizing method	△	△	△	△	△	△	—	—	△	△	△
		4.7.2	Coordinate measuring machine method	—	—	—	—	—	—	—	—	—	—	—	—	—
		4.8	Path drawing method	—	—	—	—	—	—	—	—	—	—	—	—	—

◎: These systems have the capability of calibrating both the measuring system itself and the robot base coordinate system. This also means that these systems can measure both absolute accuracy (pose, path) and relative accuracy (pose, path).

□: These systems can measure only relative accuracy (pose, path).

○: Robots with average performances can be tested with this method.

△: Performances can be measured with some limitations. See Clause 3.

For performances of each method, see Table 2.

Performance characteristics	
(1)	Pose accuracy
(2)	Pose repeatability
(3)	m-dir. Pose accuracy
(4)	Distance accuracy
(5)	Distance repeatability
(6)	Pose stabilization time
(7)	Pose overshoot
(8)	Drift of pose character.
(9)	min. Positioning time
(10)	Static compliance
(11)	Path accuracy
(12)	Path repeatability
(13)	Cornering deviations
(14)	Path velocity character.

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Table 2 Typical measuring performances of measuring methods in Table 1

Measuring methods	Instrumentation characteristics			Measuring characteristics	Maximum path velocity	Sampling rate on path measurement
	Resolution	Repeatability	Accuracy			
4.1 Positioning test probe methods	0.01 - 1 μm 0.05 % of field of view	0.001 - 0.01 mm 0.1 - 1 % of field of view	0.002 - 0.02 mm	static only	---	---
4.2.1 Mechanical gage comparison	0.025 - 0.1 mm	0.05 - 0.2 mm	0.05 - 0.2 mm	dynamic	10 m/s	0.01 ms/point
4.2.2 Laser beam path comparison	3 μm	0.02 mm	0.005 - 0.01 mm	dynamic	6 m/s	10 - 100 ms/point
4.3.1 Multi-laser tracking interferometry	0.16 μm	2 μm	0.005 - 0.01 mm	dynamic	100 - 1000 ms/p.	100 - 1000 ms/p.
4.3.2 Ultrasonic trilateration	0.05 - 1 mm	0.2 - 1 mm	0.4 - 3 mm	dynamic	5 m/s	0.5 ms/point
4.3.3 Mechanical cable trilateration	0.01 mm	0.02 mm	0.3 mm	dynamic	1 m/s	500 - 3000 ms/point
4.4.1 Single laser tracking interferometry	0.6 - 5 μm	0.005 - 0.02 mm	0.005 - 0.05 mm	dynamic	6 m/s	0.01 - 500 ms/point
4.4.2 Single total station method - tracking -	0.2 mm 5 arc-second	0.1 mm 10 arc-second	3 mm 0.5 - 1 mm	dynamic	1 m/s	500 - 3000 ms/point
4.4.3 Linear scale method	0.02 mm	0.02 mm	0.02 mm	dynamic	2 - 10 m/s	1 ms/point
4.5.1 Optical tracking triangulation	2 arc-second 0.015 %	5 arc-second	10 arc-second	dynamic	---	---
4.5.2 Theodolite method	0.1 - 0.2 arc-second	0.5 - 2 arc-second	0.5 - 2 arc-second, 1 mm	static only	---	---
4.5.3 Optical camera method	0.0005 - 0.025 % of field of view	0.001 - 0.05 % of field of view	0.01 - 0.75 % of field of view	dynamic	10 m/s	0.2 - 4 ms/point
4.6 Inertial measuring method	5 μm	0.01 mm	0.03 mm	dynamic	5 m/s	3 ms/point
4.7.1 2-D digitizing method	0.01 - 0.02 mm	0.02 - 0.2 mm	0.1 - 0.5 mm	dynamic	0.5 - 3 m/s	10 - 100 ms/p.
4.7.2 Coordinate measuring machine (floor) method	0.5 μm	5 μm	0.01 mm	static only	---	---
4.8 Path drawing method	0.2 mm	0.2 mm	0.2 - 0.5 mm	dynamic	---	---

Note 1: The data presented in this Table are based on the manufacturer's rated specifications.

The manufacturers should be consulted for verification of performance claims or description of limitations.

Note 2: Most of repeatability or accuracy values in this Table are theoretical performances when individual measuring device is installed carefully and when the dimensional stability of the entire measuring system is maintained during the measurement.

Annex A. Examples of available measuring systems/sensors

Some examples of sensors suitable for position measurement are also listed.

Measuring methods	Available systems/sensors (manufacturer, country)
4.1 Positioning test probe method	REFCUBE 6D (KRYPTON, Belgium) RPMS 200 (Sun Japan, Japan) MicroSense (ADE, USA)
4.2.1 Mechanical gage comparison method	
4.2.2 Laser beam path comparison method	ROBOTEST (Polytec, Germany)
4.3.1 Multi-laser tracking interferometry	CMS-3000 trilateration configuration (Chesapeake Laser Systems, USA) LTS-1000 (LK Tool, USA) LTCMS (Tokyo Seimitsu, Japan)
4.3.2 Ultrasonic trilateration	
4.3.3 Mechanical cable trilateration	CompuGauge (DynaLog, USA) RoboTrak (Robot Simulations, UK)
4.4.1 Single laser tracking interferometry	ROBOTEST (Polytec, Germany) SMART310 (Leica, Switzerland) CMS-3000 (Chesapeake Laser Systems, USA)
4.4.2 Single total station method (static/tracking)	static: PCM1 (Leica, Switzerland) MONMOS (Sokkia, Japan) tracking: AP-L1 (Topcon, Japan)
4.4.3 Linear scale method	
4.5.1 Optical tracking triangulation methods	OPTOTRAC (MSSR Group, University of Surrey, UK) LASERTRACE (Automatic Systems Laboratories, UK) LASER TRACKER LTS8000 (KRYPTON, Belgium)
4.5.2 Theodolite method	ECDS (Leica, Switzerland)
4.5.3 Optical camera method	MultiLab System (SELCOM AB, Sweden) RPM 9200 (Qualisys, Sweden) RODYM 6D (KRYPTON, Belgium) OPT-FOLLOW (YA-MAN Hamilton, USA) Optotrak (Northern Digital, Canada) ICAROS (iMAR GmbH, Germany) Hi-Speed Tracker×2 (EMTEC, Japan) Two-dimensional PSD S1300 (Hamamatsu Photonics, Japan)
4.6 Inertial measuring method	ICAROS (iMAR GmbH, Germany)
4.7.1 2-D digitizing method	RODYM 2.5D (KRYPTON, Belgium) PP109R (Heidenhain, Germany) MODEL 200 (Zimmer, Germany) DrawingPad (CalComp, USA)
4.7.2 Coordinate measuring machine method	Desk top CMM: GEOTIZER 500 (Mitutoyo, Japan) Portable CMM: SYSTEM 6 (ROMER, USA)
4.8 Path drawing method	

Annex B Addresses of measuring system/sensor manufacturers
(in alphabetical order)

System/sensor manufacturers	Addresses
ADE Corp. (USA)	77 Rowe Street, Newton, Massachusetts, 02166 USA
Automatic Systems Laboratories (UK)	28 Blundells Road, Bradville, Milton Keynes MK13 7HF, England
CalComp (USA)	14555 North 82nd Street, Scottsdale, Arizona, 85260 USA
Chesapeake Laser Systems, Inc. (USA)	222 Gale Lane, Kennett Square, Pennsylvania, 19348 USA
Dynalog, Inc. (USA)	2727 Second Avenue, Detroit, Michigan, 48201 USA
EMTEC (Japan)	1510-1, Kaitori, Tama-City, Tokyo, 206 Japan
Hamamatsu Photonics K.K. (Japan)	1126-1 Ichino-cho, Hamamatsu City, Shizuoka, 435 Japan
DR. JOHANNES HEIDENHAIN GmbH (Germany)	Dr.-Johannes-Heidenhain-Strasse 5, D-8225 Traunreut, Germany
iMAR GmbH (Gesellschaft für Inertiale Mess-, Automatisierungs-, und Regel-systeme mbH) (Germany)	LPA @ University of Saarland, D66041 Saarbrücken, Germany
KRYPTON Electric Eng. N.V. (Belgium)	Interleuvenlaan 86, B-3001 Leuven, Belgium
LK Tool Inc. (USA)	1625 W. University Drive, Tempe, Arizona, 85281 USA
Leica AG (Switzerland)	CH-5035 Uerzenfelden, Switzerland
Mitutoyo Corp. (Japan)	31-19, Shiba 5-chome, Minato-ku, Tokyo, 108 Japan
Northern Digital Inc. (Canada)	403 Albert Street, Waterloo, Ontario, Canada N2L 3V2
Polytec GmbH (Germany)	Postfach 161, D-76333 Waldbronn, Karlsruhe, Germany
Qualisys AB (Sweden)	Ögärdesvägen 4, S-433 30 Partille, Sweden
ROMER (USA)	806 Oakwood Boulevard, Dearborn, Michigan, 48124 USA
Robot Simulations Ltd. (UK)	Lynnwood Business Centre, Lynnwood Terrace, Newcastle upon Tyne NE4 6UL, UK
SELCOM AB (Sweden)	Box 250, S-433 25 Partille, Sweden
Sokkia Co., Ltd. (Japan)	1-1, Tomigaya 1-Chome, Shibuya-ku, Tokyo, 151 Japan
Sun Japan Corp. (Japan)	Kyokuko Bldg. 3-41-4, Nihonbashi-hamacho, Chuo-ku, Tokyo, 103 Japan
University of Surrey, MSSR Group (UK)	Guildford, Surrey GU2 5XH, England
Tokyo Seimitsu Co., Ltd. (Japan)	7-1, Shimo-Renjaku 9-chome, Mitaka, Tokyo, 181 Japan
Topcon (Japan)	75-1, Hasunuma-cho, Itabashi-ku, Tokyo, 174 Japan
YA-MAN LTD., Hamilton Lab (USA)	2005 Hamilton Avenue Suit 100, San Jose CA 95125, USA
ZIMMER GmbH (Germany)	Industriestrasse 1, D-64380 Rossdorf/Darmstadt, Germany